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## Structure Reports

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## 2-(4,5,6,7,8,9-Hexahydro-6a-azaphenyl-en-2-ylmethylene)indan-1,3-dione

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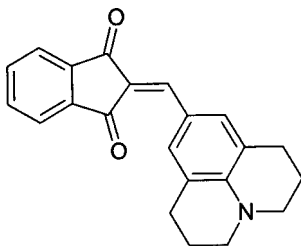
Received 19 May 2008; accepted 29 May 2008

Key indicators: single-crystal X-ray study;  $T = 293$  K; mean  $\sigma(\text{C}-\text{C}) = 0.002$  Å; disorder in main residue;  $R$  factor = 0.055;  $wR$  factor = 0.155; data-to-parameter ratio = 14.5.

The title compound,  $\text{C}_{22}\text{H}_{19}\text{NO}_2$ , has potential for use as a new nonlinear optical material. Molecules are almost planar. One C atom of the heterocyclic ring system is disordered over two positions; the site occupancy factors are 0.6 and 0.4.

### Related literature

For related literature, see: Honda *et al.* (1996); Allen (2002).



### Experimental

#### Crystal data

$\text{C}_{22}\text{H}_{19}\text{NO}_2$   
 $M_r = 329.38$

Monoclinic,  $P2_1/n$   
 $a = 8.5125$  (2) Å

$b = 19.2973$  (5) Å  
 $c = 10.4969$  (3) Å  
 $\beta = 109.5301$  (10)°  
 $V = 1625.10$  (7) Å<sup>3</sup>  
 $Z = 4$

Mo  $K\alpha$  radiation  
 $\mu = 0.09$  mm<sup>-1</sup>  
 $T = 293$  (2) K  
 $0.26 \times 0.19 \times 0.04$  mm

#### Data collection

Nonius KappaCCD diffractometer  
Absorption correction: none  
6190 measured reflections

3685 independent reflections  
2852 reflections with  $I > 2\sigma(I)$   
 $R_{\text{int}} = 0.021$

#### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.055$   
 $wR(F^2) = 0.155$   
 $S = 1.01$   
3685 reflections

255 parameters  
H-atom parameters constrained  
 $\Delta\rho_{\text{max}} = 0.27$  e Å<sup>-3</sup>  
 $\Delta\rho_{\text{min}} = -0.39$  e Å<sup>-3</sup>

Data collection: *KappaCCD Server Software* (Nonius, 1999); cell refinement: *KappaCCD Server Software*; data reduction: *DENZO* and *SCALEPACK* (Otwinowski & Minor, 1997); program(s) used to solve structure: *maXus* (Mackay *et al.*, 1999) and *SIR92* (Altomare *et al.*, 1994); program(s) used to refine structure: *maXus* and *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3* (Farrugia, 1997); software used to prepare material for publication: *SHELXL97*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RK2090).

### References

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**supplementary materials**

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## 2-(4,5,6,7,8,9-Hexahydro-6a-azaphenylene-2-ylmethylene)indan-1,3-dione

S. Belyakov, V. Kampars, P. J. Pastors and A. Tokmakov

### Comment

The molecular structure of the title compound, C<sub>22</sub>H<sub>19</sub>NO<sub>2</sub>, (**I**), with atomic numbering scheme and thermal ellipsoids is presented in Fig. 1. The indandione fragment geometry is usual. The aromatic C14-C15 and C23-C24 bonds are shorter than other aromatic bonds in yulolidine system, indicating the quinoid character. Thus, presenting schematically the structure of **I** as two mesomeric forms (A or B) one can infer that the specific weight of the ionic form of B is increased (see Fig. 2). Therefore, the deep coloration occurs for the crystals **I**. A search of the Cambridge Structural Database (CSD, Version 5.29, November 2007; Allen, 2002) indicates that there are only 26 entries containing yulolidine fragments. For the title compound there is the disorder of crystal structure analogously to the crystal structure of "Coumarin 106" (Honda *et al.*, 1996). In the yulolidine system the C17 atom is disordered and the site occupancies were initially refined then fixed at 0.6 and 0.4 for C17 and C17', respectively, in the final refinement. Atoms C17 and C17' are located on the opposite sides of the least-squares plane of the molecule. The atoms C17, C17' and C21 deviate from the molecule plane on 0.597 (4), -0.288 (6) and -0.527 (2) Å, respectively.

The packing diagram of the molecules is given in Fig. 3. The moderate  $\pi$ - $\pi$ -stacking interaction in the crystal structure of (**I**) is between pairs of inversion-related indandione systems. The five-membered cycle overlaps with the benzene ring of indandione; the centroids of these rings are separated by 3.509 (3) Å, but the distance between planes of these indandione systems is 3.435 (3) Å.

### Experimental

A mixture of indan-1,3-dione, (0.44 g, 3.0 mmole), yulolidine-9-carbaldehyde (0.62 g, 3.1 mmole) and 30 ml of absolute ethanol was boiled for 15 minutes, cooled to room temperature and filtered. Deep red crystals of **I** with metallic sheen were obtained after recrystallization from ethanol. *M.p.* is 504 K (decomp.); Yield 83%. Analysis calculated for C<sub>22</sub>H<sub>19</sub>NO<sub>2</sub>: C 80.22, H 5.81, N 4.25%; found: C 80.07, H 5.43, N 4.30%.

### Refinement

The H atoms were placed in geometrically idealized positions, with C-H distances of 0.93 Å for aromatic H atoms and 0.96 Å for other H-atoms. All H atoms were refined riding on their attached C atoms, with  $U_{iso}$  values equal to 1.2 times the  $U_{eq}$  values of the parent atoms.

## Figures

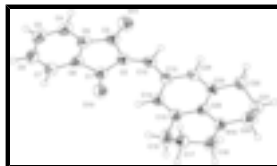


Fig. 1. The molecular structure of (**I**) with the atom numbering scheme. The displacement ellipsoids are showed at 50% probability level. H atoms are represented by spheres of arbitrary radii. Only major fragment are presented for clarity.

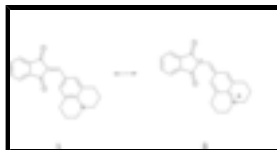


Fig. 2. Two mesomeric forms for molecular structure of **I**.

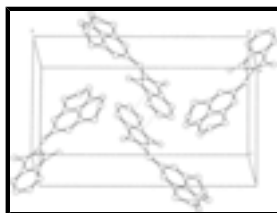


Fig. 3. Perspective view of the molecular packing for **I**, showing the stacking interactions between indandione systems.

## 2-(4,5,6,7,8,9-Hexahydro-6a-azaphenylene-2-ylmethylene)indan-1,3-dione

### Crystal data

$C_{22}H_{19}NO_2$

$M_r = 329.38$

Monoclinic,  $P2_1/n$

Hall symbol:  $-P\ 2yn$

$a = 8.5125\ (2)\ \text{\AA}$

$b = 19.2973\ (5)\ \text{\AA}$

$c = 10.4969\ (3)\ \text{\AA}$

$\beta = 109.5301\ (10)^\circ$

$V = 1625.10\ (7)\ \text{\AA}^3$

$Z = 4$

$F_{000} = 696$

$D_x = 1.346\ \text{Mg m}^{-3}$

Mo  $K\alpha$  radiation

$\lambda = 0.71073\ \text{\AA}$

Cell parameters from 6190 reflections

$\theta = 2.1\text{--}27.5^\circ$

$\mu = 0.09\ \text{mm}^{-1}$

$T = 293\ (2)\ \text{K}$

Plate, red

$0.26 \times 0.19 \times 0.04\ \text{mm}$

### Data collection

Nonius KappaCCD  
diffractometer

Radiation source: fine-focus sealed tube

Monochromator: graphite

$T = 293\ (2)\ \text{K}$

$\varphi$  and  $\omega$  scans

Absorption correction: none

6190 measured reflections

3685 independent reflections

2852 reflections with  $I > 2\sigma(I)$

$R_{\text{int}} = 0.021$

$\theta_{\text{max}} = 27.5^\circ$

$\theta_{\text{min}} = 2.1^\circ$

$h = -11 \rightarrow 11$

$k = -24 \rightarrow 23$

$l = -13 \rightarrow 13$

Refinement

|                                    |  |
|------------------------------------|--|
| Refinement on $F^2$                | Secondary atom site location: Difmap                         |
| Least-squares matrix: full         | Hydrogen site location: Geom                                 |
| $R[F^2 > 2\sigma(F^2)] = 0.055$    | H-atom parameters constrained                                |
| $wR(F^2) = 0.155$                  | Calculated $w = 1/[\sigma^2(F_o^2) + (0.0792P)^2 + 0.4361P]$ |
| $S = 1.01$                         | where $P = (F_o^2 + 2F_c^2)/3$ ?                             |
| 3685 reflections                   | $(\Delta/\sigma)_{\max} = 0.008$                             |
| 255 parameters                     | $\Delta\rho_{\max} = 0.27 \text{ e } \text{\AA}^{-3}$        |
| Primary atom site location: Direct | $\Delta\rho_{\min} = -0.39 \text{ e } \text{\AA}^{-3}$       |
|                                    | Extinction correction: none                                  |

Special details

**Geometry.** All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell s.u.'s are taken into account individually in the estimation of s.u.'s in distances, angles and torsion angles; correlations between s.u.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell s.u.'s is used for estimating s.u.'s involving l.s. planes.

**Refinement.** Refinement of  $F^2$  against ALL reflections. The weighted  $R$ -factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional  $R$ -factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating  $R$ -factors(gt) *etc.* and is not relevant to the choice of reflections for refinement.  $R$ -factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and  $R$ -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )

|     | $x$          | $y$           | $z$          | $U_{\text{iso}}^*/U_{\text{eq}}$ | Occ. (<1) |
|-----|--------------|---------------|--------------|----------------------------------|-----------|
| C1  | 1.0787 (2)   | 0.02825 (8)   | 0.26816 (16) | 0.0432 (4)                       |           |
| C2  | 0.9234 (2)   | -0.00221 (8)  | 0.27606 (15) | 0.0423 (4)                       |           |
| C3  | 0.8928 (2)   | -0.06707 (8)  | 0.19540 (17) | 0.0475 (4)                       |           |
| C4  | 1.0528 (2)   | -0.12254 (9)  | 0.04817 (18) | 0.0539 (4)                       |           |
| H4  | 0.9807       | -0.1600       | 0.0197       | 0.065*                           |           |
| C5  | 1.1874 (2)   | -0.11410 (10) | 0.00365 (19) | 0.0579 (5)                       |           |
| H5  | 1.2054       | -0.1463       | -0.0560      | 0.069*                           |           |
| C6  | 1.2957 (2)   | -0.05867 (10) | 0.04616 (19) | 0.0585 (5)                       |           |
| H6  | 1.3854       | -0.0542       | 0.0149       | 0.070*                           |           |
| C7  | 1.2720 (2)   | -0.00962 (9)  | 0.13495 (18) | 0.0526 (4)                       |           |
| H7  | 1.3447       | 0.0276        | 0.1640       | 0.063*                           |           |
| C8  | 1.1372 (2)   | -0.01783 (8)  | 0.17868 (15) | 0.0432 (4)                       |           |
| C9  | 1.0285 (2)   | -0.07358 (8)  | 0.13643 (16) | 0.0447 (4)                       |           |
| O10 | 1.15210 (15) | 0.08098 (6)   | 0.32016 (13) | 0.0576 (4)                       |           |
| O11 | 0.77589 (18) | -0.10689 (7)  | 0.17663 (15) | 0.0686 (4)                       |           |
| C12 | 0.8117 (2)   | 0.01796 (8)   | 0.33618 (15) | 0.0439 (4)                       |           |
| H12 | 0.7261       | -0.0140       | 0.3238       | 0.053*                           |           |
| C13 | 0.79509 (19) | 0.07662 (8)   | 0.41372 (15) | 0.0411 (4)                       |           |
| C14 | 0.9044 (2)   | 0.13387 (8)   | 0.44714 (17) | 0.0462 (4)                       |           |

## supplementary materials

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|      |              |              |              |             |      |
|------|--------------|--------------|--------------|-------------|------|
| H14  | 0.9949       | 0.1349       | 0.4163       | 0.055*      |      |
| C15  | 0.8815 (2)   | 0.18804 (8)  | 0.52349 (18) | 0.0471 (4)  |      |
| C16  | 0.9979 (3)   | 0.24908 (11) | 0.5566 (3)   | 0.0806 (7)  |      |
| H16A | 1.1051       | 0.2352       | 0.5539       | 0.097*      | 0.60 |
| H16B | 0.9532       | 0.2850       | 0.4912       | 0.097*      | 0.60 |
| H16C | 1.1060       | 0.2347       | 0.6147       | 0.097*      | 0.40 |
| H16D | 1.0066       | 0.2676       | 0.4744       | 0.097*      | 0.40 |
| C17  | 1.0199 (4)   | 0.27643 (19) | 0.6845 (4)   | 0.0554 (7)  | 0.60 |
| H17A | 1.0823       | 0.2443       | 0.7524       | 0.067*      | 0.60 |
| H17B | 1.0798       | 0.3194       | 0.6949       | 0.067*      | 0.60 |
| C17' | 0.9495 (7)   | 0.3072 (3)   | 0.6257 (6)   | 0.0557 (11) | 0.40 |
| H17C | 1.0477       | 0.3309       | 0.6812       | 0.067*      | 0.40 |
| H17D | 0.8808       | 0.3388       | 0.5597       | 0.067*      | 0.40 |
| C18  | 0.8574 (2)   | 0.29182 (10) | 0.7109 (2)   | 0.0615 (5)  |      |
| H18A | 0.8169       | 0.3357       | 0.6700       | 0.074*      | 0.60 |
| H18B | 0.8839       | 0.2952       | 0.8071       | 0.074*      | 0.60 |
| H18C | 0.8064       | 0.3340       | 0.7258       | 0.074*      | 0.40 |
| H18D | 0.9360       | 0.2761       | 0.7949       | 0.074*      | 0.40 |
| N19  | 0.72946 (17) | 0.23902 (7)  | 0.65742 (14) | 0.0466 (3)  |      |
| C20  | 0.5980 (2)   | 0.23753 (10) | 0.71759 (18) | 0.0531 (4)  |      |
| H20A | 0.5683       | 0.2842       | 0.7317       | 0.064*      |      |
| H20B | 0.6392       | 0.2152       | 0.8042       | 0.064*      |      |
| C21  | 0.4455 (2)   | 0.19991 (10) | 0.6302 (2)   | 0.0557 (5)  |      |
| H21A | 0.3947       | 0.2258       | 0.5486       | 0.067*      |      |
| H21B | 0.3663       | 0.1964       | 0.6771       | 0.067*      |      |
| C22  | 0.4894 (2)   | 0.12830 (9)  | 0.59526 (18) | 0.0505 (4)  |      |
| H22A | 0.5184       | 0.0996       | 0.6744       | 0.061*      |      |
| H22B | 0.3941       | 0.1081       | 0.5283       | 0.061*      |      |
| C23  | 0.63360 (19) | 0.13043 (8)  | 0.54173 (15) | 0.0405 (3)  |      |
| C24  | 0.65899 (19) | 0.07823 (8)  | 0.46198 (16) | 0.0429 (4)  |      |
| H24  | 0.5825       | 0.0420       | 0.4385       | 0.051*      |      |
| C25  | 0.74777 (18) | 0.18666 (8)  | 0.57636 (15) | 0.0386 (3)  |      |

### Atomic displacement parameters ( $\text{\AA}^2$ )

|     | $U^{11}$    | $U^{22}$    | $U^{33}$    | $U^{12}$    | $U^{13}$   | $U^{23}$    |
|-----|-------------|-------------|-------------|-------------|------------|-------------|
| C1  | 0.0486 (8)  | 0.0375 (8)  | 0.0416 (8)  | 0.0002 (6)  | 0.0127 (6) | -0.0002 (6) |
| C2  | 0.0505 (9)  | 0.0344 (7)  | 0.0408 (7)  | -0.0031 (6) | 0.0134 (7) | -0.0001 (6) |
| C3  | 0.0559 (9)  | 0.0382 (8)  | 0.0465 (9)  | -0.0039 (7) | 0.0148 (7) | -0.0019 (7) |
| C4  | 0.0628 (11) | 0.0430 (9)  | 0.0532 (10) | 0.0064 (8)  | 0.0158 (8) | -0.0053 (7) |
| C5  | 0.0709 (12) | 0.0508 (10) | 0.0529 (10) | 0.0159 (9)  | 0.0218 (9) | -0.0032 (8) |
| C6  | 0.0605 (11) | 0.0585 (11) | 0.0620 (11) | 0.0167 (9)  | 0.0278 (9) | 0.0065 (9)  |
| C7  | 0.0525 (10) | 0.0480 (9)  | 0.0580 (10) | 0.0035 (7)  | 0.0194 (8) | 0.0029 (8)  |
| C8  | 0.0482 (8)  | 0.0375 (8)  | 0.0405 (8)  | 0.0063 (6)  | 0.0104 (7) | 0.0032 (6)  |
| C9  | 0.0530 (9)  | 0.0365 (8)  | 0.0400 (8)  | 0.0052 (7)  | 0.0093 (7) | 0.0008 (6)  |
| O10 | 0.0591 (7)  | 0.0499 (7)  | 0.0697 (8)  | -0.0157 (6) | 0.0291 (6) | -0.0182 (6) |
| O11 | 0.0757 (9)  | 0.0525 (8)  | 0.0845 (10) | -0.0240 (7) | 0.0358 (7) | -0.0233 (7) |
| C12 | 0.0513 (9)  | 0.0370 (8)  | 0.0427 (8)  | -0.0083 (6) | 0.0146 (7) | -0.0002 (6) |

|      |             |             |             |              |             |              |
|------|-------------|-------------|-------------|--------------|-------------|--------------|
| C13  | 0.0462 (8)  | 0.0368 (7)  | 0.0406 (8)  | -0.0024 (6)  | 0.0148 (6)  | 0.0013 (6)   |
| C14  | 0.0438 (8)  | 0.0418 (8)  | 0.0577 (10) | -0.0031 (7)  | 0.0235 (7)  | -0.0059 (7)  |
| C15  | 0.0416 (8)  | 0.0404 (8)  | 0.0630 (10) | -0.0048 (6)  | 0.0225 (7)  | -0.0073 (7)  |
| C16  | 0.0712 (13) | 0.0601 (12) | 0.135 (2)   | -0.0293 (10) | 0.0664 (14) | -0.0441 (13) |
| C17  | 0.0490 (16) | 0.0517 (18) | 0.0645 (19) | -0.0096 (14) | 0.0176 (15) | -0.0153 (16) |
| C17' | 0.058 (3)   | 0.044 (3)   | 0.068 (3)   | -0.010 (2)   | 0.025 (2)   | -0.007 (2)   |
| C18  | 0.0574 (10) | 0.0550 (11) | 0.0747 (12) | -0.0070 (8)  | 0.0258 (9)  | -0.0237 (9)  |
| N19  | 0.0465 (7)  | 0.0460 (8)  | 0.0511 (8)  | -0.0001 (6)  | 0.0211 (6)  | -0.0054 (6)  |
| C20  | 0.0578 (10) | 0.0537 (10) | 0.0554 (10) | 0.0087 (8)   | 0.0291 (8)  | 0.0006 (8)   |
| C21  | 0.0482 (9)  | 0.0641 (11) | 0.0634 (11) | 0.0081 (8)   | 0.0299 (8)  | 0.0103 (9)   |
| C22  | 0.0479 (9)  | 0.0550 (10) | 0.0527 (9)  | -0.0050 (7)  | 0.0223 (7)  | 0.0063 (8)   |
| C23  | 0.0393 (7)  | 0.0432 (8)  | 0.0384 (7)  | -0.0009 (6)  | 0.0122 (6)  | 0.0073 (6)   |
| C24  | 0.0455 (8)  | 0.0393 (8)  | 0.0433 (8)  | -0.0078 (6)  | 0.0140 (7)  | 0.0023 (6)   |
| C25  | 0.0380 (7)  | 0.0376 (7)  | 0.0390 (7)  | 0.0029 (6)   | 0.0113 (6)  | 0.0033 (6)   |

*Geometric parameters (Å, °)*

|          |             |           |           |
|----------|-------------|-----------|-----------|
| C1—O10   | 1.2231 (19) | C17—C18   | 1.528 (4) |
| C1—C2    | 1.474 (2)   | C17—H16C  | 1.4431    |
| C1—C8    | 1.494 (2)   | C17—H17A  | 0.9600    |
| C2—C12   | 1.362 (2)   | C17—H17B  | 0.9600    |
| C2—C3    | 1.485 (2)   | C17—H17C  | 1.0804    |
| C3—O11   | 1.220 (2)   | C17—H18D  | 1.5509    |
| C3—C9    | 1.487 (2)   | C17'—C18  | 1.405 (5) |
| C4—C5    | 1.384 (3)   | C17'—H16B | 1.4854    |
| C4—C9    | 1.386 (2)   | C17'—H17B | 1.1288    |
| C4—H4    | 0.9300      | C17'—H17C | 0.9599    |
| C5—C6    | 1.385 (3)   | C17'—H17D | 0.9600    |
| C5—H5    | 0.9300      | C17'—H18A | 1.4642    |
| C6—C7    | 1.390 (3)   | C18—N19   | 1.460 (2) |
| C6—H6    | 0.9300      | C18—H18A  | 0.9600    |
| C7—C8    | 1.380 (2)   | C18—H18B  | 0.9600    |
| C7—H7    | 0.9300      | C18—H18C  | 0.9600    |
| C8—C9    | 1.391 (2)   | C18—H18D  | 0.9600    |
| C12—C13  | 1.429 (2)   | N19—C25   | 1.363 (2) |
| C12—H12  | 0.9300      | N19—C20   | 1.458 (2) |
| C13—C14  | 1.411 (2)   | C20—C21   | 1.503 (3) |
| C13—C24  | 1.412 (2)   | C20—H20A  | 0.9600    |
| C14—C15  | 1.370 (2)   | C20—H20B  | 0.9600    |
| C14—H14  | 0.9300      | C21—C22   | 1.509 (3) |
| C15—C25  | 1.423 (2)   | C21—H21A  | 0.9600    |
| C15—C16  | 1.503 (2)   | C21—H21B  | 0.9600    |
| C16—C17  | 1.396 (4)   | C22—C23   | 1.512 (2) |
| C16—C17' | 1.468 (5)   | C22—H22A  | 0.9600    |
| C16—H16A | 0.9600      | C22—H22B  | 0.9600    |
| C16—H16B | 0.9601      | C23—C24   | 1.372 (2) |
| C16—H16C | 0.9600      | C23—C25   | 1.420 (2) |
| C16—H16D | 0.9600      | C24—H24   | 0.9300    |
| C17—C17' | 0.920 (6)   |           |           |

## supplementary materials

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|                            |             |                             |             |
|----------------------------|-------------|-----------------------------|-------------|
| O10—C1—C2                  | 129.84 (15) | H16C—C17—H18D               | 144.7       |
| O10—C1—C8                  | 123.21 (15) | H17A—C17—H18D               | 73.8        |
| C2—C1—C8                   | 106.95 (13) | H17B—C17—H18D               | 106.2       |
| C12—C2—C1                  | 133.65 (15) | H17C—C17—H18D               | 100.9       |
| C12—C2—C3                  | 119.24 (14) | C17—C17 <sup>a</sup> —C18   | 79.2 (4)    |
| C1—C2—C3                   | 107.09 (14) | C17—C17 <sup>a</sup> —C16   | 67.1 (4)    |
| O11—C3—C9                  | 125.77 (15) | C18—C17 <sup>a</sup> —C16   | 117.5 (4)   |
| O11—C3—C2                  | 126.97 (17) | C17—C17 <sup>a</sup> —H16B  | 103.6       |
| C9—C3—C2                   | 107.21 (13) | C18—C17 <sup>a</sup> —H16B  | 137.5       |
| C5—C4—C9                   | 118.09 (17) | C16—C17 <sup>a</sup> —H16B  | 37.9        |
| C5—C4—H4                   | 121.0       | C17—C17 <sup>a</sup> —H17B  | 54.7        |
| C9—C4—H4                   | 121.0       | C18—C17 <sup>a</sup> —H17B  | 105.8       |
| C6—C5—C4                   | 121.28 (17) | C16—C17 <sup>a</sup> —H17B  | 95.7        |
| C6—C5—H5                   | 119.4       | H16B—C17 <sup>a</sup> —H17B | 110.1       |
| C4—C5—H5                   | 119.4       | C17—C17 <sup>a</sup> —H17C  | 70.1        |
| C5—C6—C7                   | 120.78 (18) | C18—C17 <sup>a</sup> —H17C  | 105.8       |
| C5—C6—H6                   | 119.6       | C16—C17 <sup>a</sup> —H17C  | 109.4       |
| C7—C6—H6                   | 119.6       | H16B—C17 <sup>a</sup> —H17C | 115.0       |
| C8—C7—C6                   | 117.91 (17) | H17B—C17 <sup>a</sup> —H17C | 16.5        |
| C8—C7—H7                   | 121.0       | C17—C17 <sup>a</sup> —H17D  | 175.6       |
| C6—C7—H7                   | 121.0       | C18—C17 <sup>a</sup> —H17D  | 105.0       |
| C7—C8—C9                   | 121.41 (15) | C16—C17 <sup>a</sup> —H17D  | 109.4       |
| C7—C8—C1                   | 129.00 (15) | H16B—C17 <sup>a</sup> —H17D | 72.4        |
| C9—C8—C1                   | 109.55 (14) | H17B—C17 <sup>a</sup> —H17D | 124.3       |
| C8—C9—C4                   | 120.53 (17) | H17C—C17 <sup>a</sup> —H17D | 109.5       |
| C8—C9—C3                   | 109.16 (14) | C17—C17 <sup>a</sup> —H18A  | 115.3       |
| C4—C9—C3                   | 130.25 (16) | C18—C17 <sup>a</sup> —H18A  | 39.0        |
| C2—C12—C13                 | 135.06 (15) | C16—C17 <sup>a</sup> —H18A  | 144.8       |
| C2—C12—H12                 | 112.5       | H16B—C17 <sup>a</sup> —H18A | 132.4       |
| C13—C12—H12                | 112.5       | H17B—C17 <sup>a</sup> —H18A | 114.4       |
| C14—C13—C24                | 116.46 (14) | H17C—C17 <sup>a</sup> —H18A | 103.7       |
| C14—C13—C12                | 125.41 (14) | H17D—C17 <sup>a</sup> —H18A | 69.1        |
| C24—C13—C12                | 118.14 (14) | C17 <sup>a</sup> —C18—N19   | 114.0 (2)   |
| C15—C14—C13                | 122.13 (15) | C17 <sup>a</sup> —C18—C17   | 36.3 (2)    |
| C15—C14—H14                | 118.9       | N19—C18—C17                 | 113.50 (17) |
| C13—C14—H14                | 118.9       | C17 <sup>a</sup> —C18—H18A  | 73.8        |
| C14—C15—C25                | 120.17 (14) | N19—C18—H18A                | 109.5       |
| C14—C15—C16                | 121.40 (16) | C17—C18—H18A                | 107.6       |
| C25—C15—C16                | 118.42 (15) | C17 <sup>a</sup> —C18—H18B  | 132.1       |
| C17—C16—C17 <sup>a</sup>   | 37.4 (2)    | N19—C18—H18B                | 109.5       |
| C17—C16—C15                | 112.6 (2)   | C17—C18—H18B                | 107.2       |
| C17 <sup>a</sup> —C16—C15  | 116.2 (2)   | H18A—C18—H18B               | 109.5       |
| C17—C16—H16A               | 108.1       | C17 <sup>a</sup> —C18—H18C  | 107.7       |
| C17 <sup>a</sup> —C16—H16A | 130.8       | N19—C18—H18C                | 109.5       |
| C15—C16—H16A               | 109.6       | C17—C18—H18C                | 132.9       |
| C17—C16—H16B               | 107.9       | H18A—C18—H18C               | 37.8        |
| C17 <sup>a</sup> —C16—H16B | 72.0        | H18B—C18—H18C               | 74.4        |
| C15—C16—H16B               | 109.1       | C17 <sup>a</sup> —C18—H18D  | 106.6       |
| H16A—C16—H16B              | 109.5       | N19—C18—H18D                | 109.5       |



|                            |           |               |             |
|----------------------------|-----------|---------------|-------------|
| C17—C16—H16C               | 72.9      | C17—C18—H18D  | 73.1        |
| C17 <sup>a</sup> —C16—H16C | 106.0     | H18A—C18—H18D | 136.5       |
| C15—C16—H16C               | 109.8     | H18B—C18—H18D | 37.8        |
| H16A—C16—H16C              | 38.7      | H18C—C18—H18D | 109.5       |
| H16B—C16—H16C              | 136.9     | C25—N19—C20   | 121.36 (14) |
| C17—C16—H16D               | 134.2     | C25—N19—C18   | 122.09 (14) |
| C17 <sup>a</sup> —C16—H16D | 106.1     | C20—N19—C18   | 115.42 (14) |
| C15—C16—H16D               | 109.2     | N19—C20—C21   | 112.15 (14) |
| H16A—C16—H16D              | 73.6      | N19—C20—H20A  | 109.2       |
| H16B—C16—H16D              | 38.7      | C21—C20—H20A  | 109.2       |
| H16C—C16—H16D              | 109.5     | N19—C20—H20B  | 109.2       |
| C17 <sup>a</sup> —C17—C16  | 75.6 (4)  | C21—C20—H20B  | 109.2       |
| C17 <sup>a</sup> —C17—C18  | 64.5 (4)  | H20A—C20—H20B | 107.9       |
| C16—C17—C18                | 114.2 (2) | C20—C21—C22   | 110.93 (14) |
| C17 <sup>a</sup> —C17—H16C | 110.3     | C20—C21—H21A  | 109.5       |
| C16—C17—H16C               | 39.5      | C22—C21—H21A  | 109.5       |
| C18—C17—H16C               | 147.7     | C20—C21—H21B  | 109.5       |
| C17 <sup>a</sup> —C17—H17A | 172.0     | C22—C21—H21B  | 109.5       |
| C16—C17—H17A               | 109.5     | H21A—C21—H21B | 108.0       |
| C18—C17—H17A               | 107.5     | C23—C22—C21   | 111.32 (14) |
| H16C—C17—H17A              | 76.6      | C23—C22—H22A  | 109.4       |
| C17 <sup>a</sup> —C17—H17B | 73.7      | C21—C22—H22A  | 109.4       |
| C16—C17—H17B               | 109.3     | C23—C22—H22B  | 109.4       |
| C18—C17—H17B               | 106.9     | C21—C22—H22B  | 109.4       |
| H16C—C17—H17B              | 101.5     | H22A—C22—H22B | 108.0       |
| H17A—C17—H17B              | 109.5     | C24—C23—C25   | 118.88 (14) |
| C17 <sup>a</sup> —C17—H17C | 56.7      | C24—C23—C22   | 121.31 (14) |
| C16—C17—H17C               | 107.3     | C25—C23—C22   | 119.79 (14) |
| C18—C17—H17C               | 92.2      | C23—C24—C13   | 123.41 (14) |
| H16C—C17—H17C              | 111.9     | C23—C24—H24   | 118.3       |
| H17A—C17—H17C              | 125.4     | C13—C24—H24   | 118.3       |
| H17B—C17—H17C              | 18.2      | N19—C25—C15   | 120.18 (14) |
| C17 <sup>a</sup> —C17—H18D | 98.3      | N19—C25—C23   | 120.98 (14) |
| C16—C17—H18D               | 140.3     | C15—C25—C23   | 118.83 (14) |
| C18—C17—H18D               | 36.3      |               |             |

Fig. 1

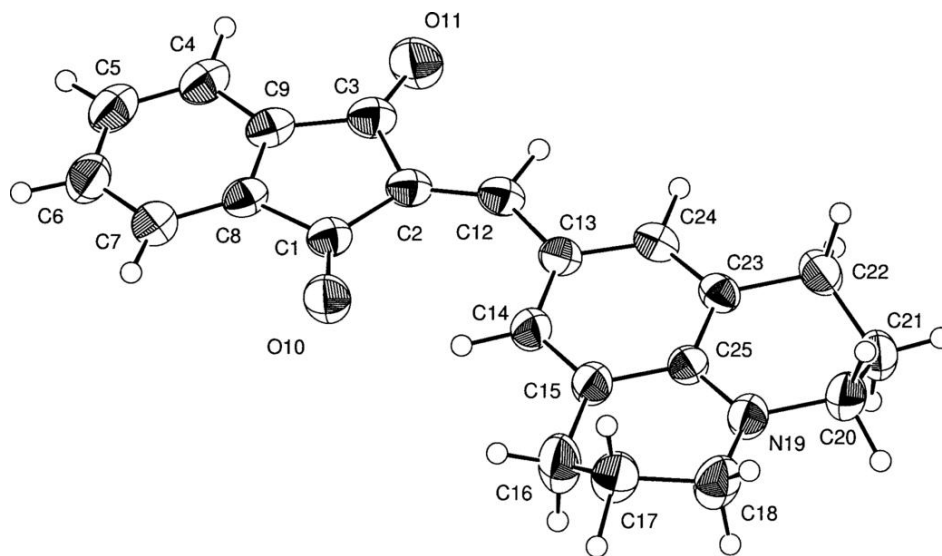


Fig. 2

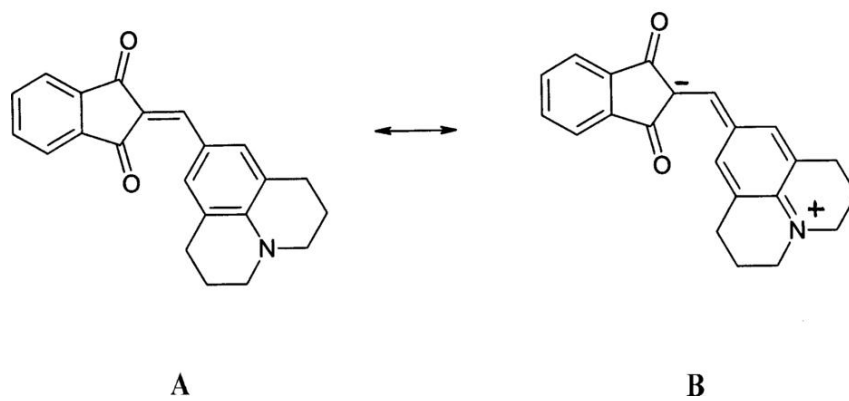


Fig. 3

